



Europäisches Patentamt
European Patent Office
Office européen des brevets



(11) **EP 1 063 334 A1**

(12) **EUROPEAN PATENT APPLICATION**

(43) Date of publication:
27.12.2000 Bulletin 2000/52

(51) Int. Cl.⁷: **D04H 5/04**

(21) Application number: **00304544.0**

(22) Date of filing: **26.05.2000**

(84) Designated Contracting States:
**AT BE CH CY DE DK ES FI FR GB GR IE IT LI LU
MC NL PT SE**
Designated Extension States:
AL LT LV MK RO SI

(30) Priority: **22.06.1999 GB 9914499**

(71) Applicant:
**JOHNSON MATTHEY PUBLIC LIMITED
COMPANY**
London **SW1Y 5BQ (GB)**

(72) Inventors:
• **Brown, Karen Leanne**
Sonning Common, Reading RG4 9RU (GB)
• **Gascoyne, John Malcolm**
High Wycombe, Bucks HP14 4BB (GB)

(74) Representative:
Wishart, Ian Carmichael et al
Patents Department
Johnson Matthey Technology Centre
Blount's Court
Sonning Common
Reading, RG4 9NH (GB)

(54) **Non-woven fibre webs**

(57) A non-woven fibre web comprising a plurality of first fibres of amorphous silica, said first fibres being orientated in the x-, y- and optionally z-direction, and optionally being bonded with one or more binder substances, characterised in that one or more continuous strands are embedded within the non-woven fibre web, each continuous strand comprising one or more second fibres of amorphous silica, and a method for the manufacture thereof is disclosed. Also disclosed is an ion-conducting membrane comprising said non-woven web and the use thereof, in particular, in a fuel cell.

EP 1 063 334 A1

Description

[0001] The present invention relates to a novel non-woven fibre web with continuous reinforcing strands, a membrane comprising said web and a membrane electrode assembly comprising said membrane, all of which have application in electrochemical devices, for example for use in a fuel cell. The invention further describes a process for the manufacture of the web, membrane and membrane electrode assembly.

[0002] Electrochemical cells invariably comprise at their fundamental level a solid or liquid electrolyte and two electrodes, the anode and cathode, at which the desired electrochemical reactions take place. A fuel cell is an energy conversion device that efficiently converts the stored chemical energy of its fuel into electrical energy by combining either hydrogen, stored as a gas, or methanol stored as a liquid or gas, with oxygen to generate electrical power. The hydrogen or methanol is oxidised at the anode and the oxygen is reduced at the cathode of the electrochemical cell. In these cells gaseous reactants and/or products have to be diffused into and/or out of the cell electrode structures. The electrodes therefore are specifically designed to be porous to gas diffusion in order to optimise the contact between the reactants and the reaction sites in the electrode to maximise the reaction rate. The electrolyte which has to be in contact with both electrodes to maintain electrical contact in the fuel cell may be acidic or alkaline, liquid or solid, in nature. The proton exchange membrane fuel cell (PEMFC) is the most likely type of fuel cell to find wide application as a more efficient and lower emission power generation technology in a range of markets including stationary and portable power devices and as alternative to the internal combustion engine in transportation. In the PEMFC, whether hydrogen or methanol fuelled, the electrolyte is a solid proton conducting polymer membrane, commonly based on perfluorosulphonic acid materials.

[0003] In the PEMFC the combined laminate structure formed from the membrane and the two electrodes is known as a membrane electrode assembly (MEA). The MEA will typically comprise several layers, but can in general be considered, at its basic level, to have five layers, which are defined principally by their function. On either side of the membrane an anode and cathode electrocatalyst is incorporated to increase the rates of the desired electrode reactions. In contact with the electrocatalyst containing layers, on the opposite face to that in contact with the membrane, are the anode and cathode gas diffusion substrate layers. The anode gas diffusion substrate is designed to be porous and to allow the reactant hydrogen or methanol to enter from the face of the substrate exposed to the reactant fuel supply, and then to diffuse through the thickness of the substrate to the layer which contains the electrocatalyst, usually platinum metal based, to maximise the electrochemical oxidation of hydrogen or methanol. The anode electrocatalyst layer is also designed to comprise some level of the proton conducting electrolyte in contact with the same electrocatalyst reaction sites. With acidic electrolyte types the product of the anode reaction are protons and these can then be efficiently transported from the anode reaction sites through the electrolyte to the cathode layers. The cathode gas diffusion substrate is also designed to be porous and to allow oxygen or air to enter the substrate and diffuse through to the electrocatalyst layer reaction sites. The cathode electrocatalyst combines the protons with oxygen to produce water and is also designed to comprise some level of the proton conducting electrolyte in contact with the same electrocatalyst reaction sites. Product water then has to diffuse out of the cathode structure. The structure of the cathode has to be designed such that it enables the efficient removal of the product water. If water builds up in the cathode, it becomes more difficult for the reactant oxygen to diffuse to the reaction sites, and thus the performance of the fuel cell decreases. In the case of methanol fuelled PEMFCs, additional water is present due to the water contained in the methanol, which can be transported through the membrane from the anode to the cathode side. The increased quantity of water at the cathode requires removal. However, it is also the case with proton conducting membrane electrolytes, that if too much water is removed from the cathode structure, the membrane can dry out and the performance of the fuel cell also decreases.

[0004] The complete MEA can be constructed by several methods. The electrocatalyst layers can be bonded to one surface of the gas diffusion substrates to form what is known as a gas diffusion electrode. The MEA is then formed by combining two gas diffusion electrodes with the solid proton-conducting membrane. Alternatively, the MEA may be formed from two porous gas diffusion substrates and a solid proton-conducting polymer membrane catalysed on both sides (hereinafter referred to as a catalyst coated membrane or CCM); or indeed the MEA may be formed from one gas diffusion electrode and one gas diffusion substrate and a solid proton-conducting polymer catalysed on the side facing the gas diffusion substrate.

[0005] Conventionally, the solid proton conducting membrane electrolytes used in the PEMFC and other devices are selected from commercially available membranes, for example perfluorinated membranes sold under the trade names Nafion® (E.I. DuPont de Nemours and Co.), Aciplex® (Asahi Chemical Industry) and Flemion® (Asahi Glass KK). For application in the PEMFC the membranes are typically below 200µm in thickness to provide a high level of ionic conductivity. However, for the advanced, high power density fuel cells, these need to have membranes less than 100µm thick and preferably less than 50µm thick. It is also necessary with these membranes that a high level of water is present within the membrane to provide efficient proton hydration and a high proton conductivity. The dimensional changes that occur as the level of water content (hydration) of the membrane changes are a particular problem during fabrication of the MEA as the stresses set up by changes in hydration during the conventionally employed thermal bond-

ing process can be so large as to break the bond between the catalyst and the membrane, or the catalyst and the substrate. Furthermore, the dimensional changes that occur due to the changes in the level of hydration of the membrane lead to considerable difficulties in handling membranes during the fabrication of large area MEAs (for example greater than 500cm²). The thinner the membrane, the more difficult the handling becomes.

[0006] To address these problems composite membrane structures have been prepared. With thicker types of membrane (e.g. >350µm) developed for other applications, it has been possible to incorporate 'macro' reinforcing materials such as woven polytetrafluoroethylene (PTFE) to minimise such dimensional changes. However, these thicker materials have too low an ionic conductivity to be of use in the PEMFC. US. Patent 5,547,551 assigned to W.L. Gore & Associates Inc. describe the fabrication of ultra-thin composite membranes below 25µm in thickness which comprise incorporating proton conducting polymer material into an expanded porous PTFE membrane. According to Kolde et al., Electrochemical Society Proceedings Vol. 95-23, p193-201 (1995), the composite membrane shows a considerably lower reduction in tensile strength on hydration and much improved dimensional stability compared to the conventional non-reinforced membranes. The material has, however, a higher specific resistance (lower ionic conductivity) than an unmodified pure proton conducting membrane such as Nafion® 117 by a factor of at least two.

[0007] The higher specific resistance of the above composite membrane means that in practice it has to be much thinner than the equivalent pure proton conducting membrane to maintain the same overall conductivity and thus cell performance. However, reducing the thickness of the composite membrane reduces the advantages that a composite membrane can provide. For example, there is a limit to the extent to which the thickness of the membrane can be reduced since as the membrane is made thinner, the durability and longevity can decrease, and reactant gas cross-over through the membrane is more liable to occur, both of which lead to a reduction in the cell performance. Furthermore, the problems associated with dimensional stability and handlability for MEA fabrication can be exacerbated with thinner membranes. The use of a thermoplastic polymer to produce the composite also means that during MEA fabrication both the ion conducting polymer and the reinforcing polymer will flow under pressure.

[0008] E.I. DuPont de Nemours and Co. (WO95/16730) describe a process for making a reinforced substantially non-porous membrane with satisfactory mechanical strength and very low resistance to ionic conduction which approaches that of very thin, unreinforced perfluoro ion exchange polymer membranes. The composite membrane utilises a porous hydrocarbon substrate, such as a polyolefin, and on which at least one side is coated with an ion exchange film formed from a fluorinated polymer. However, again the use of a thermoplastic polymer to produce the reinforcing component of the composite raised the potential for localised thinning as a consequence of plastic flow during MEA fabrication.

[0009] For PEMFC's to become commercially viable power sources over a wide range of applications, the membrane will require a manufacturing process capable of producing millions of square metres of material at low cost and able to impart specific structural properties to the material for each application. One recent approach to a composite membrane structure, which does not compromise ionic conductivity and allows the fabrication of thin membranes (200 microns or less) has utilised a porous substrate of non-woven fibres as the matrix into which is embedded an ion conducting polymer (EP 0 875 524 A2). Additional modifications to the structure of the fibre matrix have enabled the characteristics of the final membrane to be more tightly controlled as disclosed in PCT patent applications PCT/GB99/02935 and PCT/GB99/03277. However, to produce membranes in very large volumes requires the development of large volume reel to reel processes, as these offer the most attractive route for the manufacture of the membrane. Consequently it will be necessary for the porous fibre structure to be produced as a continuous sheet of material (a web) which has sufficient strength to be machine processed at relatively high speeds. Typically webs of the type described in the aforementioned applications, because of their open structure, limited thickness and relatively fragile materials of construction, have low tensile strengths. Indeed for many applications, membranes below 100 microns thick are an attractive option with the requirement for a fibre web that is thinner than the final membrane. Hence fibre web thicknesses of 50 microns or less are likely to be required for applications requiring high power density. It is therefore an object of the present invention to overcome the disadvantages of current porous fibre webs for membrane production. A further object of the present invention is to provide a process for the manufacture of the fibre web of the invention, in particular a process that is capable of producing the fibre web in high volumes and with high yields and at low unit cost, and preferably as a single continuous process. A still further object is to provide a process for preparing a membrane in high volumes and with high yields and at low unit cost.

[0010] Accordingly, the present invention provides a non-woven fibre web comprising a plurality of first fibres of amorphous silica, said first fibres being orientated in the x-, y- and optionally z-direction, and optionally being bonded with one or more binder substances, characterised in that one or more continuous strands are embedded within the sub-surface layer of the non-woven fibre web, each continuous strand comprising one or more second fibres of amorphous silica.

[0011] The amorphous silica for use in the web according to the invention is to be distinguished from crystalline quartz, although there is a tendency in an industrial context for the terms "quartz" and "silica" to be used interchangeably. Although both are chemically silicon dioxide, quartz is the crystalline form and is both hard and brittle, whereas the

fibrous materials (the amorphous silica for use in the substrate of the invention) are made from either natural or synthetic quartz, and are amorphous and glass like in character, having no crystalline structure.

[0012] The one or more second fibres in the one or more continuous strands may be present as a single fibre, or as a plurality of fibres in the form of a tow or yarn. A tow is an essentially parallel collection of synthetic fibres preparatory to spinning, and a yarn is a continuous twisted strand of two or more fibres. When two or more continuous strands are embedded within the sub-surface layer of the web, the fibre(s) in each continuous strand may be a single fibre, or a plurality of fibres in the form of a tow or yarn, or a combination thereof.

[0013] The first fibres are suitably selected from the group consisting of longer fibres and shorter fibres, or a combination of longer and shorter fibres. The longer fibres are of average length greater than 3mm and suitably have a maximum average length of 50mm. The preferred average length of the fibres is 5mm to 30mm. The diameter of the longer fibres is typically in the range of 0.2 microns to 25 microns, preferably in the range of 2 microns to 20 microns. The shorter fibres have an average length of less than 3mm, suitably are of average length less than 2mm, preferably less than 1mm. The shorter fibres have a minimum length of 50 microns, preferably 100 microns. The diameter of the shorter fibres is typically in the range 0.1 microns to 20 microns, preferably 0.4 microns to 10 microns.

[0014] The first fibres in the non-woven fibre web are held together by the one or more binder substances (the "final binder"), which may be a polymeric material or an inorganic metal oxide such as silica. Depending on the binder substance(s) used it may also contribute to the essential membrane properties of the MEA, such as water movement within the membrane. Examples of such binder substances include:

- (i) non-ion conducting polymers, (such as polytetrafluoroethylene (PTFE), fluorinated ethylene-propylene (FEP), polyvinylidene difluoride (PVDF), Viton A, polyethylene, polypropylene, ethylene-propylene),
- (ii) ion-conducting polymers, (such as Nafion[®]),
- (iii) colloidal silica, and
- (iv) other metal oxides and hydroxides, (such as zirconia and titania) or any combination thereof.

[0015] The or each continuous strand is embedded within the sub-surface layer of the non-woven fibre web. When more than one continuous strand is present, each continuous strand may be at an equal depth or at varying depths (i.e. variation in the z-direction) or a combination thereof. The continuous strand(s) may be applied at any orientation and at any spacing. The continuous strand(s) may also have applied to the surface of, or impregnated within, the strands a non-ion conducting polymer or polymers or an ion-conducting polymer or polymers or a combination of the two. Examples of such polymers include polytetrafluoroethylene (PTFE), fluorinated ethylene-propylene (FEP), polyvinylidene difluoride (PVDF), Viton A, polyethylene, polypropylene, ethylene-propylene and Nafion[®].

[0016] The or each continuous strand(s) are made up of one or more second fibres of amorphous silica. The number of fibres in each strand will depend on the required thickness of the web and the application for which it is to be used. The maximum length of the second fibres is determined by the dimensions of the web and the orientation of the continuous strand within the web. For example, the continuous strand may extend from one edge of the web to any one of the other edges, or the continuous strand may extend from one edge of the web to the same edge. In all cases, the length of the second fibre(s) will be dependent on the length of the continuous strand. The diameter of the second fibre(s) is typically in the range of 0.1 to 50 microns, suitably 0.2 microns to 20 microns. The final cross-section profile of the strand(s) within the web will depend on the number and thickness of fibres in the strand and the final thickness of the web.

[0017] The non-woven fibre web may be made by a single individual processor by adapting a continuous manufacturing process, such as paper making, to form a continuous web. In both cases the first fibres are dispersed as a suspension in, preferably water, to form a slurry. Also optionally added to the slurry are one or more binder substances (the "first binder"), such as hydrophilic polymers, for example polyvinylalcohol (PVA). The first binder may be in the form of fibres. Once first fibres and the optional first binder are uniformly dispersed in the liquid, the resultant slurry is drained through a suitable mesh in order to form a coherent layer of the non-woven fibre web. In the case of a single individual process the fibres are deposited onto a mesh in a conventional hand sheet maker the deposition process being carried as a series of layers, the continuous strands being introduced onto the required deposited layer so that each strand or group of strands is placed at the desired level within the final sheet. When formed into a continuous structure by the controlled deposition of the slurry onto a moving mesh belt the continuous strands are introduced onto the deposited layer at the appropriate point in the deposition process so that each strand is placed at the desired level within the web. The sheet or web so-formed by either process is dried in an oven to set the first binder. If necessary the sheet or web is placed in a solution of the final binder, which may or may not be the same as the first binder, allowed to dry and optionally heat-treated to set the final binder. If it is not desirable for the first binder to remain in the final web structure, it may be removed by this heat treatment or by an alternative appropriate process. In addition, any undesirable residues may be removed by the heat treatment or by an alternative appropriate process.

[0018] A second embodiment of the invention provides an ion-conducting membrane comprising a non-woven web

as hereinbefore described and a filler material, characterised in that the filler material comprises an ion conducting polymer. The ion-conducting membrane of the invention has a final thickness of less than 200µm, suitably less than 100µm, and preferably less than 50 µm.

[0019] For PEM fuel cell applications, the ion conducting polymer is a proton conducting polymer, examples of such polymers being well known to those skilled in the art. More than one proton conducting polymer may be present and/or a non-ion conducting polymer may also be included in the novel membrane of the invention.

[0020] The proton conducting polymers suitable for use in the present invention may include, but are not limited to:

1) Polymers which have structures with a substantially fluorinated carbon chain optionally having attached to it side chains that are substantially fluorinated. These polymers contain sulphonic acid groups or derivatives of sulphonic acid groups, carboxylic acid groups or derivatives of carboxylic acid groups, phosphonic acid groups or derivatives of phosphonic acid groups, phosphoric acid groups or derivatives of phosphoric acid groups and/or mixtures of these groups. Perfluorinated polymers include Nafion[®], Flemion[®] and Aciplex[®] commercially available from E. I. DuPont de Nemours (U.S. Patents 3,282,875; 4,329,435; 4,330,654; 4,358,545; 4,417,969; 4,610,762; 4,433,082 and 5,094,995), Asahi Glass KK and Asahi Chemical Industry respectively. Other polymers include those covered in U.S. Patent 5,595,676 (Imperial Chemical Industries plc) and US. Patent 4,940,525 (Dow Chemical Co.)

2) Perfluorinated or partially fluorinated polymers containing aromatic rings such as those described in WO 95/08581, WO 95/08581 and WO 97/25369 (Ballard Power Systems) which have been functionalised with SO₃H, PO₂H₂, PO₃H₂, CH₂PO₃H₂, COOH, OSO₃H, OPO₂H₂, OPO₃H₂. Also included are radiation or chemically grafted perfluorinated polymers, in which a perfluorinated carbon chain, for example, PTFE, fluorinated ethylene-propylene (FEP), tetrafluoroethylene-ethylene (ETFE) copolymers, tetrafluoroethylene-perfluoroalkoxy (PFA) copolymers, poly (vinyl fluoride) (PVF) and poly (vinylidene fluoride) (PVDF) is activated by radiation or chemical initiation in the presence of a monomer, such as styrene, which can be functionalised to contain an ion exchange group.

3) Fluorinated polymers such as those disclosed in EP 0 331 321 and EP 0345 964 (Imperial Chemical Industries plc) containing a polymeric chain with pendant saturated cyclic groups and at least one ion exchange group which is linked to the polymeric chain through the cyclic group.

4) Aromatic polymers such as those disclosed in EP 0 574 791 and US Patent 5,438,082 (Hoechst AG) for example sulphonated polyaryletherketone. Also aromatic polymers such as polyether sulphones which can be chemically grafted with a polymer with ion exchange functionality such as those disclosed in WO 94/16002 (Allied Signal Inc.).

5) Nonfluorinated polymers include those disclosed in US. Patent 5,468,574 (Dais Corporation) for example hydrocarbons such as styrene-(ethylene-butylene)-styrene, styrene-(ethylene-propylene)-styrene and acrylonitrile-butadiene-styrene co- and terpolymers where the styrene components are functionalised with sulphonate, phosphoric and/or phosphonic groups.

6) Nitrogen containing polymers including those disclosed in US. Patent 5,599,639 (Hoechst Celanese Corporation), for example, polybenzimidazole alkyl sulphonic acid and polybenzimidazole alkyl or aryl phosphonate.

7) Any of the above polymers which have the ion exchange group replaced with a sulphonyl chloride (SO₂Cl) or sulphonyl fluoride (SO₂F) group rendering the polymers melt processable. The sulphonyl fluoride polymers may form part of the precursors to the ion exchange membrane or may be arrived at by subsequent modification of the ion exchange membrane. The sulphonyl halide moieties can be converted to a sulphonic acid using conventional techniques such as, for example, hydrolysis.

[0021] Other non-ion conducting polymeric materials which may be used in addition to the one or more ion conducting or proton conducting polymers include PTFE, FEP, PVDF, Viton[®] and hydrocarbon types such as polyethylene, polypropylene and polymethylmethacralate.

[0022] Other ion-conducting polymeric materials which are not proton conducting polymers may be used in the filler material. For example, such polymers can be used for applications requiring a bipolar membrane or a completely anion exchange membrane. Anion exchange polymers are generally based on quaternary ammonium groups, rather than the fixed sulphonic acid groups in proton conducting polymers. These include, for example, the tetraalkyl ammonium group (-N⁺R₃) and the quaternary ammonium centre in Tosflex[®] membranes (-N(R₁)(CH₂)_yN⁺(R₃)) supplied by Tosoh. However, it can be envisaged that all of the proton exchange polymers described above could have anion exchange equivalents.

[0023] The polymer is suitably applied to the non-woven fibre web in the form of a solution, the solvents of which may be either organic or aqueous based. Solvents of all of the above polymers may include or may be modified to include, water, methanol and/or other aliphatic alcohols, ethers, acetone, tetrahydrofuran (THF), n-methylpyrrolidone (NMP), dimethyl sulphoxide (DMSO) dimethyl formamide (DMF) dimethyl acetamide (DMAc) or protonic solvents such as sulphuric acid or phosphoric acid and/or mixtures of the above. However, it has been found that an essentially aqueous solution of the polymer as described in EP 0 731 520 is preferred.

[0024] It may also be beneficial to incorporate particulate materials within the membrane to increase either the sites

available for proton migration and/or to increase the sites available for holding water within the substrate. Materials such as silica, titanium dioxides, zirconium oxides, zirconium silicates, tungsten oxides, tin oxides and zeolites with a mean particle size of 0.001 μ m to 10 μ m, preferably 0.01 μ m to 5 μ m are examples of suitable particulates which may be used. The particulate material may first be coated, for example, with an ion conducting polymer, a non-conducting hydrophobic or hydrophilic polymer, or a catalyst.

[0025] The membranes may be manufactured by taking a non-woven fibre web as hereinbefore described and thereafter applying the polymeric material. This can be done by any number of coating processes such as thin-film casting, dip coating, spraying, printing, rolling, K-bar, or doctor blade methods. Alternatively, a continuous manufacturing process similar to that used to prepare the non-woven fibre web may be used, the filler material being added to the slurry.

[0026] The present invention also provides a catalyst coated membrane comprising a membrane as hereinbefore described and a method for the manufacture thereof. A further aspect of the present invention relates to a membrane electrode assembly comprising a membrane as hereinbefore described and a method for the manufacture thereof. A still further aspect of the present invention relates to a fuel cell comprising a membrane as hereinbefore described. Alternatively, the invention relates to a fuel cell comprising a catalyst coated membrane as hereinbefore described. Alternatively, the invention relates to a fuel cell comprising a membrane electrode assembly as hereinbefore described.

[0027] The present invention is not limited to the use of the non-woven fibre web or membrane in a fuel cell, and any electrochemical or other device which comprises a web or membrane of the invention is within the scope. Other applications for which one or more of the embodiments of the invention may be used, in addition to fuel cells, include, but are not limited to, metal-air batteries, electrochemical gas sensors, electrochemical reactors for the electrosynthesis of useful chemical compounds and separator mats for batteries. Non-electrochemical applications of the non-woven fibre web include, but are not limited to, composite materials for cryogenic insulation, composite reinforcement in areas such as plastics, cements, printed circuit boards, sports goods etc, for insulation purposes, military applications, automotive structural components, brakes, gaskets, transmission units etc and for filtration applications.

[0028] The present invention will now be described by way of example only, which is not intended to be limiting thereof.

Comparative Example 1

[0029] A mixture of chopped silica fibres (Type QC9/33-20mm from Quartz et Silice BP 521- 77794 Nemours, Cedex, France) 0.37g, and silica microfibre (Q fibre, type 104 from Johns Manville, Insulation Group, PO Box 5108, Denver, CO, USA) 0.18g were dispersed with mixing, in water (3000 cm³). A porous network was fabricated from the resulting mixture in a single step process based on the principles of paper-making technology, as a sheet size of 855 cm² (33cm diameter) in a sheet former (design based on standard SCA Sheet former from AB Lorentzen & Wettre, Box 4, S-163 93 Stockholm, Sweden). The porous fibre sheet was removed from the wire and air dried at 150°C.

Comparative Example 2

[0030] A mixture of chopped silica fibres (Type QC9/33-20mm) 0.37g, and silica microfibre (Q fibre, type 104) 0.18g were formed into a sheet as for Comparative Example 1.

[0031] The porous fibre sheet was sprayed with a binder solution comprising a 5% solution of Nafion[®], 1100 EW in lower aliphatic alcohols (Solutions Technologies Inc., Mendenhall, PA 19357, USA) to give a dry Nafion[®] loading of 0.78g.

Comparative Example 3

[0032] A mixture of chopped silica fibres (Type QC9/33-20mm) 0.37g, and silica microfibre (Q fibre, type 104) 0.18g were formed into a sheet as for Comparative Example 1. The fibre sheet, as formed on the wire and whilst still wet, was sprayed with a binder solution comprising a 20wt% solution of colloidal silica (Ludox[®] AS 40; DuPont Speciality Chemicals, Havennummer 500, Wilmington Straat, 2030 Antwerp, Belgium) to give a loading of 0.1g of the silica. The sheet was removed from the wire and air dried at 150°C.

Example 1

[0033] A mixture of chopped silica fibres (Type QC9/33-20mm from Quartz et Silice BP 521- 77794 Nemours, Cedex, France) 0.185g, and silica microfibre (Q fibre, type 104 from Johns Manville, Insulation Group, PO Box 5108, Denver, CO, USA) 0.09g were dispersed with mixing, in water (3000 cm³). A porous fibre network was fabricated from the resulting mixture in a single step process as for Comparative Example 1. The porous fibre sheet was left on the wire.

A series of straight lengths of silica yarn (Quartzel yarn C9 17Z20 QS13 supplied by Quartz et Silice BP 521- 77794 Nemours, Cedex, France) were spaced at 0.5cm intervals across the surface of the porous fibre sheet using a jig to maintain them in place under tension. The hand sheet maker was carefully refilled with water. A further mixture of chopped silica fibres (Type QC9/33-20mm) 0.185g, and silica microfibre (Q fibre, type 104) 0.09g were dispersed with mixing, in water (3000 cm³), dispersed in the sheet maker and deposited on the existing porous fibre sheet and yarn. The sheet was removed from the wire and air dried at 150°C.

Example 2

[0034] A porous fibre sheet with silica yarn at 0.5cm spacings was formed as in Example 1. The sheet was removed from the wire and air dried at 150°C.

[0035] The porous fibre sheet was sprayed with a binder solution comprising a 5% solution of Nafion®, 1100 EW in lower aliphatic alcohols (Solutions Technologies Inc., Mendenhall, PA 19357, USA) to give a dry Nafion® loading of 0.78g.

Example 3

[0036] A porous fibre sheet with silica yarn at 0.5cm spacings was formed as in Example 1. The fibre sheet, as formed on the wire and whilst still wet, was sprayed with a binder solution comprising a 20wt% solution of colloidal silica (Ludox® AS 40; DuPont Speciality Chemicals, Haverhill, MA 01830, USA) to give a loading of 0.1g of the silica. The sheet was removed from the wire and air dried at 150°C.

[0037] Test samples of size 20mm x 100mm were cut from the sheets prepared in Comparative Examples 1 to 3 and Examples 1 to 3. In the case of Examples 1, 2 and 3 the samples were orientated such that the silica yarn was aligned in the 100mm length direction. The samples were evaluated for their tensile strength using a Hounsfield H5K-S Materials Testing Machine fitted with soft faced jaws and a 5N load cell for Comparative Examples 1 to 3 and a 100N load cell for Examples 1 to 3. With all of the samples rather than exhibiting a break at the maximum stress (i.e. the tensile strength) the webs tended to show, beyond the maximum stress, elongation and a significant reduction in the stress. This reflected a significant loss in the strength of the web materials due to the untangling of the silica fibres. The relative strength of the samples was, therefore, compared in terms of the maximum stress (i.e. the stress at yield) and the force at which the maximum stress was evident (i.e. the force at yield). The results are presented in Table 1.

Table 1

Stress at yield and force at yield for the webs			
Sample	Average Thickness μm	Stress at Yield Pa $\times 10^8$	Force at Yield N
Comparative Example 1	30	0.06	0.035
Comparative Example 2	30	7.5	4.5
Comparative Example 3	30	1.1	0.66
Example 1	45	19	17
Example 2	45	40	36
Example 3	45	16	14

[0038] A web formed from just a mixture of the chopped and microfine silica as in Comparative Example 1 shows a very low stress and force at yield of 0.06×10^8 Pa and 0.035 N respectively. With this strength the web would be far too weak to handle on a reel to reel machine. The incorporation of single lengths of silica yarn at a spacing of 0.5 cm into the structure, as shown by Example 1, results in an increase in the stress and force at yield of over two orders of magnitude to 19×10^8 Pa and 17 N respectively. The silica yarn has produced a web that is sufficiently strong to be handleable in a reel to reel process.

[0039] As can be seen from Table 1 by comparing Comparative Examples 2 and 3 with Comparative Example 1, the addition of Nafion or silica binders to the web does result in a significant increase in the stress and force at yield. However, the strength of the webs with the binders is still too low to envisage handling them in a reel to reel process. The inclusion of silica yarn into the webs containing the binders produces, however, a further significant improvement in the stress and force at yield. With Nafion binder Comparative Example 2 shows a stress and force at yield of 7.5×10^8 Pa and 4.5 N respectively. The addition of silica yarn to this web in Example 2, at a spacing of 0.5 cm, increases

the stress and force at yield to 40×10^8 Pa and 36 N respectively. Correspondingly, in Comparative Example 3, with silica binder the web shows a stress and force at yield of 1.1×10^8 Pa and 0.66 N respectively. The addition of silica yarn to this web in Example 3, at a spacing of 0.5 cm, increases the stress and force at yield to 16×10^8 Pa and 14 N respectively. These increases in the strength of the webs containing the binders, by the addition of silica yarn, results in the production of webs that are sufficiently strong to be suitable for use in the reel to reel processes that are commonly employed in volume manufacture.

Claims

1. A non-woven fibre web comprising a plurality of first fibres of amorphous silica, said first fibres being orientated in the x-, y- and optionally z-direction, and optionally being bonded with one or more binder substances, characterised in that one or more continuous strands are embedded within the non-woven fibre web, each continuous strand comprising one or more second fibres of amorphous silica.
2. A non-woven web according to claim 1 wherein the continuous strands embedded within the web may be at equal depths or varying depths or a combination thereof.
3. A non-woven web according to any preceding claim, wherein the one or more continuous strand(s) have a polymer applied to the surface of, or impregnated within, the strands.
4. A non-woven web according to any preceding claim, wherein the diameter of the second fibres is in the range of 0.1 microns to 50 microns.
5. A non-woven web according to any preceding claim, wherein the first fibres are selected from the group consisting of longer fibres and shorter fibres.
6. A non-woven web according to claim 5, wherein the longer fibres are of average length greater than 3 mm.
7. A non-woven web according to claim 5, wherein the shorter fibres are of average length less than 3 mm.
8. An ion-conducting membrane comprising a non-woven fibre web according to any one of claims 1 to 7 and a filler material, characterised in that the filler material comprises an ion-conducting polymer.
9. A membrane according to claim 8 wherein the ion-conducting polymer is a proton conducting polymer.
10. A membrane according to claim 8 or claim 9, wherein the filler material further comprises a non-ion-conducting polymer.
11. A membrane according to any one of claims 8 to 10, wherein the filler material further comprises one or more particulate materials.
12. A membrane according to claim 11, wherein the one or more particulate materials are first coated with an ion-conducting polymer, a non-ion-conducting hydrophobic or hydrophilic polymer, or a catalyst.
13. A catalyst coated membrane comprising a membrane according to any one of claims 8 to 12.
14. A membrane electrode assembly comprising a membrane according to any one of claims 8 to 12.
15. A fuel cell comprising a membrane according to any one of claims 8 to 12.
16. A fuel cell comprising a catalyst coated membrane according to claim 13.
17. A fuel cell comprising a membrane electrode assembly according to claim 14.



European Patent
Office

EUROPEAN SEARCH REPORT

Application Number
EP 00 30 4544

DOCUMENTS CONSIDERED TO BE RELEVANT			
Category	Citation of document with indication, where appropriate, of relevant passages	Relevant to claim	CLASSIFICATION OF THE APPLICATION (Int.Cl.7)
D,Y	EP 0 875 524 A (JOHNSON MATTHEY PLC) 4 November 1998 (1998-11-04) * column 3, line 22 - column 8, line 12; claims 12,7,9-12, *	1,2,5-17	D04H5/04
Y	US 2 731 066 A (HOGENDOBLER ET AL. 2) 17 January 1956 (1956-01-17) * column 1, line 20 - column 2, line 42 *	1,2,5-17	
A	DE 16 19 026 A (FA. CARL FREUDENBERG) 21 August 1969 (1969-08-21) * page 2, line 1, paragraph 3 - page 5, line 7, paragraph 1 *	1,8	
A	WO 94 16134 A (MINNESOTA MINING & MFG) 21 July 1994 (1994-07-21) * page 12, line 1 - line 19; claims 1,20,23 *	1	
The present search report has been drawn up for all claims			TECHNICAL FIELDS SEARCHED (Int.Cl.7) D04H H01M
Place of search THE HAGUE		Date of completion of the search 11 October 2000	Examiner V Beurden-Hopkins, S
CATEGORY OF CITED DOCUMENTS X : particularly relevant if taken alone Y : particularly relevant if combined with another document of the same category A : technological background O : non-written disclosure P : intermediate document T : theory or principle underlying the invention E : earlier patent document, but published on, or after the filing date D : document cited in the application L : document cited for other reasons & : member of the same patent family, corresponding document			

EPO FORM 1503 03.82 (PatCat)

**ANNEX TO THE EUROPEAN SEARCH REPORT
ON EUROPEAN PATENT APPLICATION NO.**

EP 00 30 4544

This annex lists the patent family members relating to the patent documents cited in the above-mentioned European search report. The members are as contained in the European Patent Office EDP file on
The European Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

11-10-2000

Patent document cited in search report		Publication date	Patent family member(s)		Publication date
EP 0875524	A	04-11-1998	JP	10312815 A	24-11-1998
			US	6042958 A	28-03-2000
<hr/>					
US 2731066	A	17-01-1956	NONE		
<hr/>					
DE 1619026	A	21-08-1969	NONE		
<hr/>					
WO 9416134	A	21-07-1994	CA	2152085 A	21-07-1994
			DE	69305096 D	31-10-1996
			DE	69305096 T	30-04-1997
			EP	0678128 A	25-10-1995
			JP	8505442 T	11-06-1996
			NO	952693 A	07-07-1995
			US	5380580 A	10-01-1995
<hr/>					

EPO FORM P4439

For more details about this annex : see Official Journal of the European Patent Office, No. 12/82